

Exercise 1: Pressure Sensor

This problem set is intended to be a walk through the design and operation of a silicon pressure sensor. The pressure sensor is made of highly boron doped resistors standing on a silicon oxide film to eliminate the p-n junctions and therefore increase the operating temperature range of silicon based pressure sensors as shown in Figure 1.

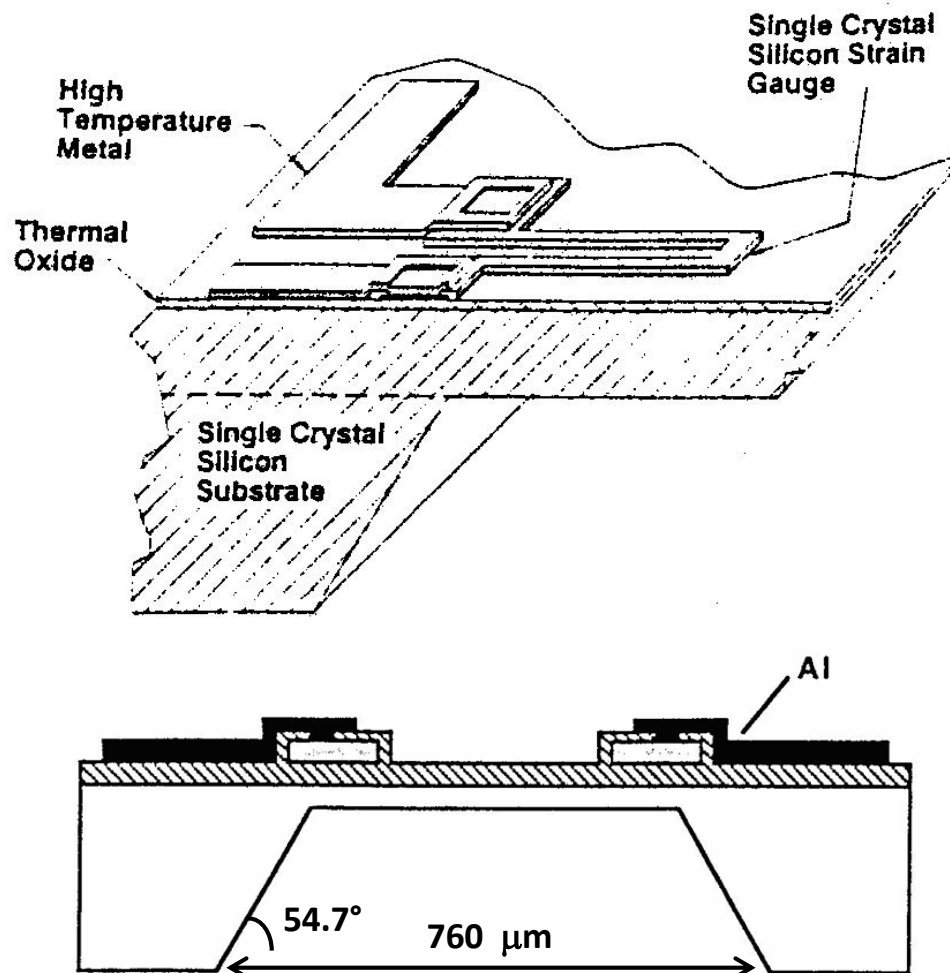


Figure 1: Cutaway view and cross-section of single-crystal silicon resistors standing on a silicon membrane passivated with a silicon oxide film.

Some characteristics:

- Wafer thickness of $275\ \mu\text{m}$.
- The silicon membrane has a thickness of $20\ \mu\text{m}$.
- The piezoresistors thickness is $1.0\ \mu\text{m}$.

MASK LAYOUT - PRESSURE TRANSDUCER

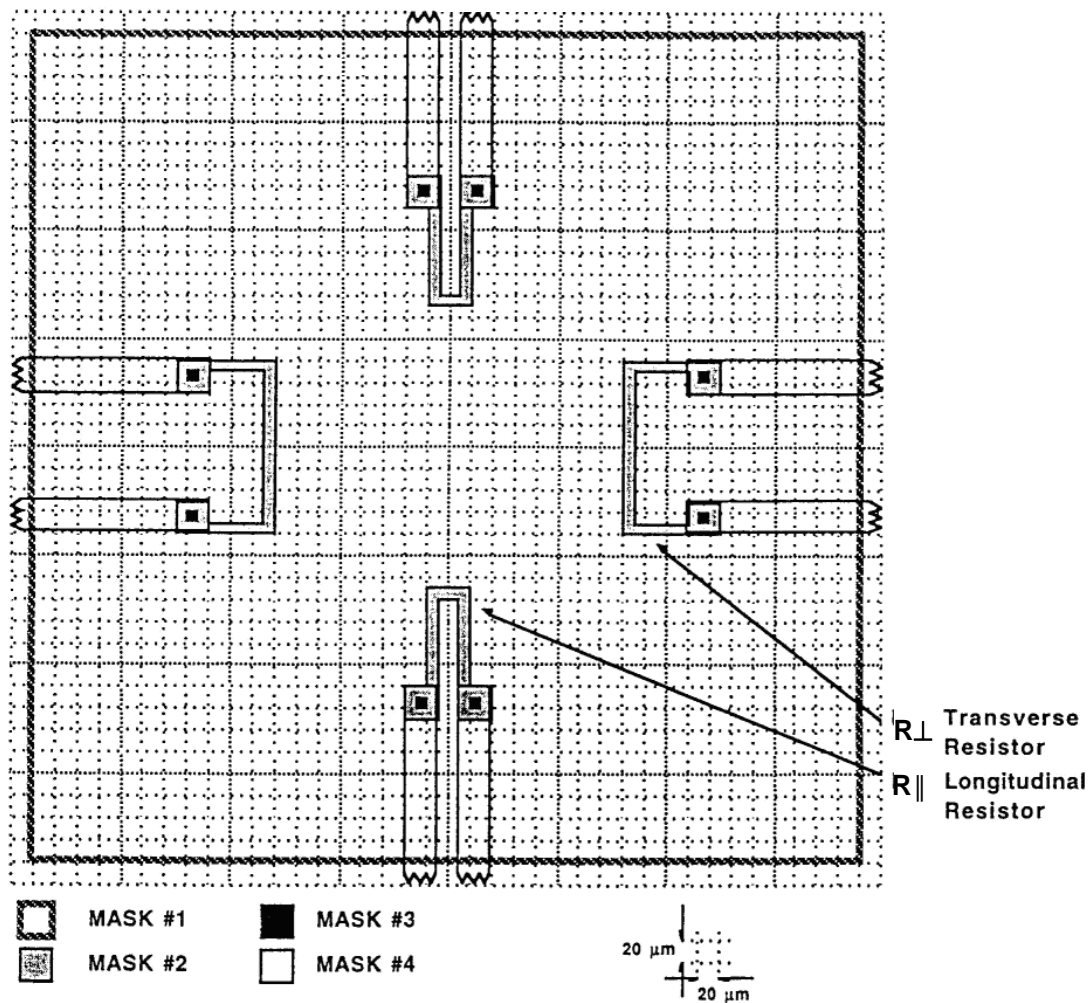


Figure 2: Layout of the pressure sensor using a 4 masks fabrication process.

- a) What is the criteria to define the location of the piezoresistors on the silicon membrane ?

Answer: Region with the higher stress. For a clamped square membrane, this region is near the edges of the membrane.

- b) Why are the piezoresistors positioned in two different orientations, R_{\perp} and R_{\parallel} .

Answer: To have opposite variations of their resistance value for implementation in a Wheatstone bridge for the read-out circuit.

- c) On Figure 2 draw the edges of the silicon membrane.

Answer: Membrane is a $400 \times 400 \text{ } \mu\text{m}^2$ square with the piezoresistors on the inner side of the membrane and their contacts on the outside.

- d) Complete the section below on the characteristics of the pressure sensor fabricated using the mask layout presented in Figure 2. (thickness of piezoresistors: $1 \text{ } \mu\text{m}$, $\rho \text{ Si} = 0.001 \text{ } \Omega\text{-cm}$).

Membrane thickness: $20 \text{ } \mu\text{m}$

Membrane edge length: $400 \text{ } \mu\text{m}$

Sheet resistance of the silicon used for the Si piezoresistors: $10 \text{ } \Omega/\square$

Sheet resistance = $0.001 \text{ } \Omega\text{-cm} / 10^{-4} \text{ cm}$

Values of the two transversal and longitudinal piezoresistors:

$R_{\perp} = \underline{190 \text{ } \Omega}$ (18 squares + $4 \times \frac{1}{4}$ square for the corners)

$R_{\parallel} = \underline{250 \text{ } \Omega}$ (24 squares + $4 \times \frac{1}{4}$ square for the corners)

- e) Using this pressure transducer, we will determine the expected resistor change due to an applied pressure. Some expressions are given to you below to solve the following questions.

For silicon: $\frac{E}{1-\nu^2} = 200 \text{ GPa}$,

For a square diaphragm, the deformation at the centre is:

$$w = 1.638 \times 10^{-3} \frac{12(1-\nu^2)}{E} \bullet \frac{l^4}{h^3} P$$

$$\sigma_{\perp} = \frac{0.294 \times l^2 \times P}{h^2} \quad \sigma_{\parallel} = \frac{0.115 \times l^2 \times P}{h^2}$$

$$\frac{\Delta R_{\parallel}}{R_{\parallel}} = \pi_{\parallel} \sigma_{\parallel} + \pi_{\perp} \sigma_{\perp} \approx \frac{1}{2} \pi_{44} (\sigma_{\parallel} - \sigma_{\perp})$$

$$\frac{\Delta R_{\perp}}{R_{\perp}} = \pi_{\parallel} \sigma_{\perp} + \pi_{\perp} \sigma_{\parallel} \approx \frac{1}{2} \pi_{44} (\sigma_{\perp} - \sigma_{\parallel})$$

Assuming an applied pressure of 2.5 MPa and $\frac{1}{2}(\pi_{44}) = 36 \times 10^{-11} \text{ Pa}^{-1}$:

- i) What is the deflection in the middle of the diaphragm?

Answer: $w = 0.786 \text{ } \mu\text{m}$

- ii) Determine the longitudinal and the transverse stress at the centre of the diaphragm edge where the piezoresistors are located.

Answer: $\sigma_{\parallel} = 115 \text{ MPa}$ $\sigma_{\perp} = 294 \text{ MPa}$

- iii) What is the fractional change in resistance for a 2.5 MPa load for resistors placed in parallel and perpendicular to the diaphragm edge?

$$\Delta R_{\parallel} / R_{\parallel} = -0.064 = \alpha \quad \Delta R_{\perp} / R_{\perp} = 0.064 = \beta$$

- f) Assume that the resistors are configured as a full Wheatstone bridge (see drawing below).

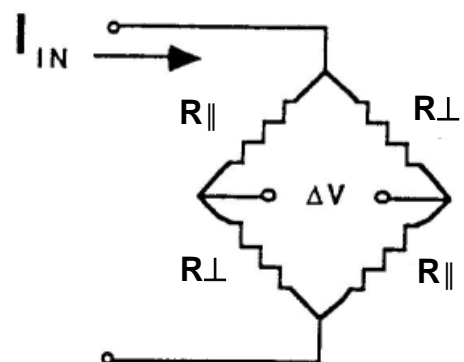
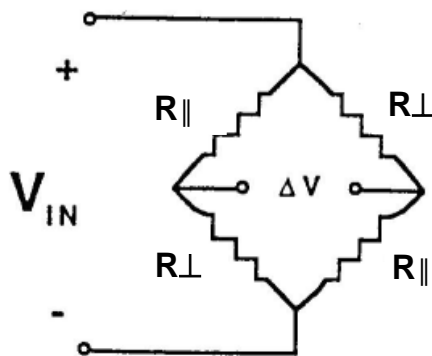
- i) Determine an expression for the differential output voltage from this circuit for a change in pressure, P , as a function of R_{\parallel} and R_{\perp} . Derive the expression for both constant voltage drive and constant current drive, as shown below.

$$Z = (R_{\perp} - R_{\parallel})/2$$

Answer: Z: Bridge's input impedance

$$\Delta V = \left(\frac{R_{\perp} - R_{\parallel}}{R_{\perp} + R_{\parallel}} \right) V_{\text{IN}}$$

$$\Delta V = (R_{\perp} - R_{\parallel}) I_{\text{IN}} / 2$$



- ii) Is either mode, constant current / constant voltage, preferred?

Answer: Contact voltage non-linear relationship, constant current has the advantage to result in a linear relationship.

- iii) Using the resistance values from the previous questions, what is the output voltage for a 2.5 MPa load? Assume that V_{IN} and I_{IN} are chosen such that the static power dissipation is less than 10 mW.

$$\text{Answer: } 10 \text{ mW} = Z \times I_{IN}^2 \quad I_{IN} = 6.75 \text{ mA and } V_{IN} = 1.5 \text{ V}$$

$$R_{||} = R_{||,0} (1+\alpha) \quad \text{and} \quad R_{\perp} = R_{\perp,0} (1+\beta)$$

$$\Delta V_{out} = \Delta V_{(2.5 \text{ MPa})} - \Delta V_{(0 \text{ MPa})}$$

$$\Delta V_{out} = [R_{\perp,0} (1+\beta) - R_{||,0} (1+\alpha)] \times I_{IN}/2 - [R_{\perp,0} - R_{||,0}] \times I_{IN}/2$$

$$\Delta V_{out} = [R_{\perp,0} \times \beta - R_{||,0} \times \alpha] \times I_{IN}/2 = 95 \text{ mV for } 2.5 \text{ MPa} = 0.038 \text{ } \mu\text{V} / \text{Pa}$$

- iv) Estimate the minimum detectable pressure if the dominant noise source is thermal noise in the resistors. Assume a bandwidth of 10 kHz.
- $$v = \sqrt{4kTR\Delta f}$$

$$\text{Answer: } R = 250 \text{ } \Omega \quad \Delta f = 10 \text{ kHz} \quad T = 23^\circ\text{C} \Rightarrow v = 0.2 \text{ } \mu\text{V}$$

Minimum detectable voltage is defined as twice the noise: 0.4 μV which corresponds to 10 Pa (using the answer in question f)iii above.

- g) Estimate the effect of the following variables on the sensitivity of the sensor.

- i) $\pm 5 \text{ } \mu\text{m}$ wafer thickness variation.

Answer: In equation of σ , variation of thickness of 5 μm on a total membrane thickness of 20 μm represents a change of about a factor 2 for σ . This results in a variation of $\pm \sim 50\%$ of change in sensitivity.

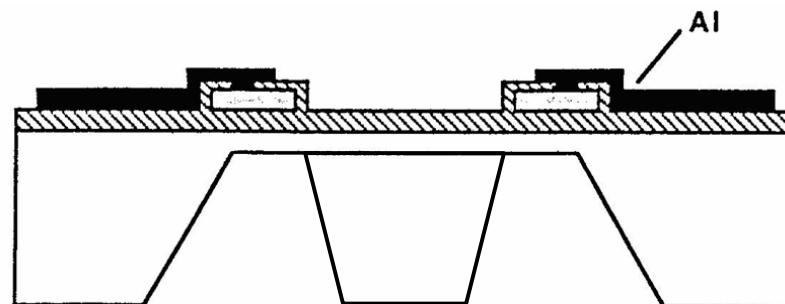
- ii) $\pm 1 \text{ } \mu\text{m}$ line width variation.

Answer: This will cause a $\pm 10\%$ variation of the piezoresistors values resulting in a $\pm 10\%$ variation in sensitivity.

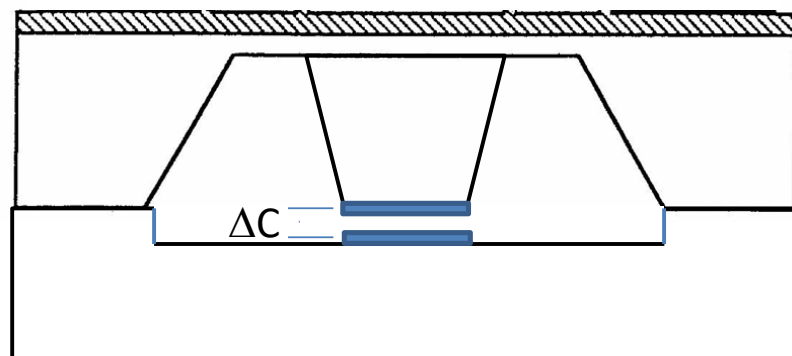
Exercise 2: Accelerometer

- a) Using the piezoresistive principle, what would you change to the configuration of the pressure sensor in exercise one to make a piezoresistive accelerometer?

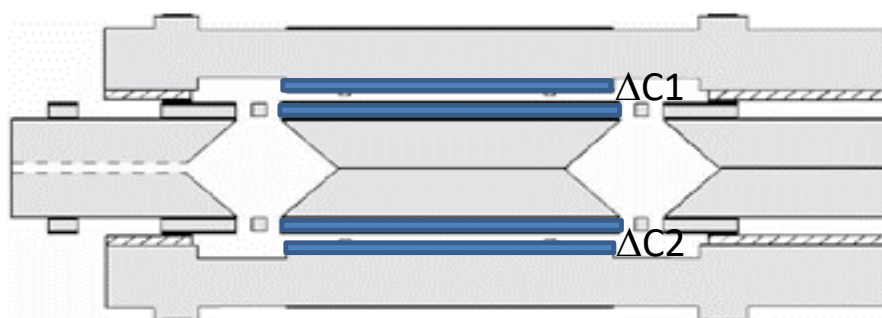
Answer: Add a proof mass for higher sensitivity (higher force and higher stress on the piezoresistors area).



- b) And using the same configuration as in a) how would you implement capacitive transduction? And if you would like to perform a differential capacitive measurement?

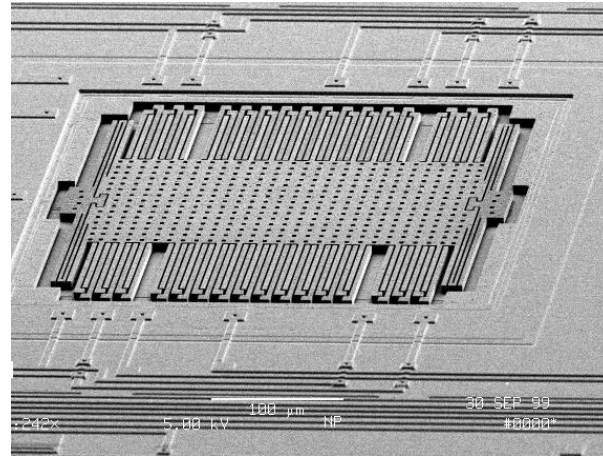


Differential configuration: Capacitive accelerometer from Colibrys



- c) What is currently the mainly used capacitive transducer configuration in MEMS accelerometers?

Answer: Comb electrodes for capacitive differential sensing. There is a set of stationary fingers and a set of fingers that move under acceleration. See slides 25 to 32 from Lecture 2 on MEMS sensors part1.



Exercise 3: Gyroscope

- a) Describe the implementation of a MEMS gyroscope using a schematic drawing.

Answer: See slides 73 to 79 from Lecture 2 on MEMS Sensors part1.

- b) Give the name and the expression of the force that will result in a displacement of the structure due to an angular rotation.

Answer: Coriolis force with m: mass, v: speed of the mass, Ω : angular rate of rotation

$$\begin{aligned} \vec{F}_C &= 2m(\vec{v} \times \vec{\Omega}) \\ &= -2m(\vec{\Omega} \times \vec{v}) \end{aligned}$$

- c) Which parameters can you play with to increase the sensitivity of the gyroscope response? And how these should be optimised for higher sensitivity.

Answer: Weight of the masses and their velocity. Increase of mass and increase of velocity (increase of the driving frequency of the comb drive actuation of the masses)